

Nanoscale Electromagnetic Compatibility: Quantum Coupling and Matching in Nanocircuits

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Abstract—The paper investigates two typical electromagnetic compatibility (EMC) problems, namely, coupling and matching in nanoscale circuits composed of nano-interconnects and quantum devices in entangled state. Nano-interconnects under consideration are implemented by using carbon nanotubes or metallic nanowires (NWs), while quantum devices by semiconductor quantum dots. Equivalent circuits of such nanocircuits contain additional elements arising at nanoscale due to quantum effects. As a result, the notions of coupling and impedance matching are reconsidered. Two examples are studied: in the first one, electromagnetically coupled NWs are connected to classical lumped devices; in the second one, electromagnetically uncoupled transmission lines are terminated on quantum devices in entangled states. In both circuits, the EMC features qualitatively and quantitatively differ from their classical analogs. In the second example, we demonstrate the existence of quantum coupling, due to the entanglement, which exists in spite of the absence of classical electromagnetic coupling. The entanglement also modifies the matching condition introducing a dependence of the optimal value of load impedance on the line length.

Index Terms—Electromagnetic compatibility (EMC), kinetic inductance, nanocircuits, nanoelectromagnetism, quantum devices, quantum entanglement.

I. INTRODUCTION

TODAY'S achievements of nanoelectronics allow utilization and manipulation of small collections of atoms and molecules, such as semiconductor heterostructures, quantum wells, quantum wires and quantum dots [1]–[3], different forms

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of nanocarbon (spherical fullerenes, graphene, and carbon nanotubes (CNTs) [4]–[7]), noble metal nanowires (NWs) [8], organic macromolecules, and organic polymers [9]. The increasingly intensive penetration of nanotechnologies lead to the birth of the so-called “nanoelectromagnetism” [10], [11], a novel branch of applied science related to the interaction of electromagnetic radiation with quantum mechanical low-dimensional systems.

One of the crucial aspects of electromagnetism for electronic devices and systems is related to their electromagnetic compatibility, i.e., of their ability to operate successfully, with controlled levels of emissions and with a suitable degree of robustness to unwanted electromagnetic couplings via various mechanisms of interference [12]–[14].

However, with the transition of electronics to nanoscale, new physical phenomena as well as new materials' properties need to be studied. Quantum effects, such as discrete energy spectrum of charge carriers, existence of phonons, ballistic transport and tunneling, many-body correlations, interface effects, and so on, manifest themselves jointly with classical electromagnetic interactions [15], [16]. As a result, the classical design based on the phenomenological separate analysis of physical properties of electric circuit elements and functional properties of devices and systems becomes invalid with respect to nanoelectronics. These considerations lead to the conclusion that the “classical” EMC, completely based on macroscopic electrodynamics, must be deeply revised starting from the basic concepts and opening the era of “nano-EMC” [17]–[19].

For instance, the classical scaling rules used to design integrated circuits (ICs) and to implement EMC solutions are based on the macroscopic behavior of the electrical parameters, such as inductances and capacitances. However, the quantum terms appearing in the models of nanoelectronics change the dependence of such electrical parameters on frequency, geometry, and temperature. Consequently, the classical EMC concepts like coupling, shielding, and matching should be reconsidered, along with the classical solutions to such issues. In other words, nano-EMC poses new challenges in modeling devices and systems, establishing new design rules, and assessing reliable characterization procedures.

Nano-EMC modeling assumes the self-consistent solution of Maxwell's equations with the quantum transport equations for charge carriers. Transition from the macroscopic to the atomic scale can be performed via either of the three distinct approaches to electron transport modeling: classical, semiclassical, and quantum. Many works were devoted to this topic, investigating

nanomaterials for EMC applications like shielding [20], [21], modeling the interactions between EM fields and nanostructures [22], [23], and modeling nano-interconnects [24]–[29].

The classical approach, with the most limited validity area, is the simplest one. For example, Drude model of conductivity in metals [16] considers the conducting electron as a classical particle, which moves in the electric field while encountering inelastic collisions with a randomly vibrating ion lattice.

The semiclassical approach is based on the concept of a particle ensemble behaving as a nonideal gas with quantum effects taken into account by replacing the real particle mass by the corresponding effective value [15], [16]. In these models, electrons are unable to tunnel through barriers. In collision events, the electrons' scattering is inelastic, thus the kinetic energy of incident particles is not conserved. The transmission line (TL) model for CNT interconnects presented in [28] and [29] may be noted as an example of such a semiclassical approach.

On the contrary, at the molecular or atomic scale, a quantum approach is needed, since the transport is governed by the wave-like behavior of the electrons. Thus, unwanted interactions between elements exist both due to electromagnetic coupling and quantum phenomena, such as tunneling, spin–orbit interaction, and various many-body effects, including dipole–dipole and spin–spin interactions. As a result, appears the entanglement of quantum states, which produces the long-living and long-distance correlations of quantum origin in electric circuits [16]. For their descriptions, the complete Maxwell–Schrödinger model is necessary. One of the most convenient forms of it is based on the concept of generalized susceptibilities (Kubo approach) [16].

This paper discusses the concepts of *coupling* and *matching* in a nanoscale signaling system composed of NWs connecting quantum devices in the entangled states. The interest in this type of systems from the EMC point of view stems mainly from their potential as digital elements for quantum computing and quantum informatics [1]. In particular, the paper compares predictions of the conventional EMC theory with those of nano-EMC taking into account the coupling of quantum nature, due to the entanglement.

The paper is organized as follows. Section II is devoted to the modeling. First, the TL model for nano-interconnects based on metal NWs or CNTs is briefly recalled. Then, an equivalent lumped model to describe a pair of quantum devices in entangled state is proposed. Section III deals with the analysis of two complementary case studies: the first one refers to a nano-interconnect with a crosstalk noise induced by an unwanted electromagnetic coupling. The second proposes two uncoupled NWs terminated on two quantum dots in the entangled state. The summary and conclusive remarks are given in Section IV.

II. MODELING A NANOSCALE SIGNALING SYSTEM

In this paper, we analyze the behavior of signaling nanocircuits composed of quantum devices connected by NWs, which play a role of transmission lines. Section II-A summarizes the quasi-classical model of transport in NWs made of metals or

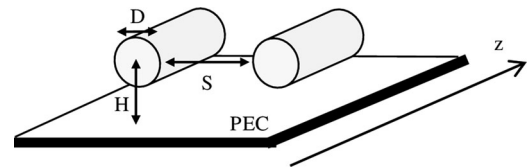


Fig. 1. Reference geometry for the nano-interconnect: two signal lines above a perfect electric conducting (PEC) ground.

CNTs, presented in [28], [29], and [32], while Section II-B proposes an equivalent lumped model of the quantum devices in the entangled state, in the framework of the circuit theory.

A. Modeling Nanoscale Interconnects

The considered nano-interconnect (see Fig. 1) is based on the two signal lines suspended in air above a perfectly conducting ground. The interconnect length is assumed infinite in the z -direction. This model adequately describes a real interconnect if the diameters of the signal lines are much smaller than their lengths (typically, at least an order of magnitude). The conducting material for the signal lines may either be a metallic NW or a CNT. The wire diameter is assumed to be large enough (at least 1 nm) for having a local crystal structure of the wire, which allows the using of *semiclassical transport model*. For assumed ratio between diameter and length, the conducting NW can be regarded as a one-dimensional (1-D) material, with the charge transport characterized by two quantum-confined directions and single one unconfined.

The operating frequencies range is from zero up to some THz so that:

- 1) the cross-section diameter D of both NWs is electrically small;
- 2) the manifestations of transverse currents in the NWs may be neglected;
- 3) only the intraband transitions in the particle movement are taken into account.

Since the conducting electrons are laterally quantum confined, they occupy the narrow energy subbands, instead of the ordinary wide bands found in the bulk materials. Along the longitudinal axis, the lattice exhibits translational symmetry and is long enough to consider the longitudinal electron wavenumber as a continuous value. Such type of energy spectrum may be evaluated by means of the *tight-binding approximation* (e.g., CNTs [30]) or the first principle calculations (e.g., copper NWs [31]).

In the semiclassical approximation, the electrons are considered as a 1-D gas described by the Boltzmann transport equation. The quantum nature of the conductive electrons is accounted via a nonparabolic dispersive law [28], [29].

In the momentum domain, the traveling wave can be presented as $\exp\{i(\omega t - \beta z)\}$, where ω is the radian frequency and β is the wavenumber. By solving the transport equation in such a domain, we get the following expression for the longitudinal component of the current density \hat{J}_z [28], [29]:

$$\hat{J}_z(\beta, \omega) = \hat{\sigma}_{zz}(\beta, \omega) \hat{E}_z(\beta, \omega) \quad (1)$$

where \hat{E}_z is the longitudinal component of the electric field and $\hat{\sigma}_{zz}$ is the longitudinal conductivity. The latter can be evaluated as the sum of all the contributions of the sub-bands

$$\hat{\sigma}_{zz}(\beta, \omega) = \sum_{\mu=1}^N \hat{\sigma}_{\mu}. \quad (2)$$

Here, the number N refers to the subbands that significantly contribute to the conduction, namely, those for which the energy gap with respect to the Fermi level is small enough, usually $|E_{\mu} - E_F| \leq 5k_B T$, where E_F and E_{μ} are, respectively, the energies of the Fermi level and of the μ th energy subband (in eV), T is the absolute temperature, and k_B the Boltzmann constant (in eV/K). Assuming the collision frequency ν to be constant for all the sub-bands close to the Fermi level, it results

$$\hat{\sigma}_{zz}(\beta, \omega) \cong -i \frac{2e^2 v_F}{\pi X \hbar} \frac{1}{\omega - i\nu} M \left[1 - \xi(\omega) \left(\frac{v_F \beta}{\omega - i\nu} \right)^2 \right]^{-1} \quad (3)$$

where \hbar is the reduced Planck constant, v_F is the Fermi velocity, M is the equivalent number of conducting channels [28], and the quantities X and $\xi(\omega)$ depend on the material used as signal trace. For the case of CNT, the quantity X is its circumference and [32]

$$X = \pi D, \quad \xi(\omega) = 1 \quad (4)$$

while for an NW, X is its cross section S_W and [33]

$$X = S_W = \frac{\pi}{4} D^2, \quad \xi(\omega) = \frac{1}{3} \left(\frac{1 + 1.8i\omega/\nu}{1 + i\omega/\nu} \right). \quad (5)$$

By combining (3) and (1), we get a *generalized Ohm's law*

$$[1 - \psi(\omega)\beta^2] \hat{J}_z(\beta, \omega) = \frac{\sigma_0}{1 + i\omega/\nu} \hat{E}_z(\beta, \omega) \quad (6)$$

where

$$\psi(\omega) = \frac{\xi(\omega)v_F^2}{\nu^2(1 + i\omega/\nu)^2} \quad (7)$$

$$\sigma_0 = \frac{2v_F M}{\nu R_0 X} \quad (8)$$

and $R_0 = \pi\hbar/e^2 = 12.9 \text{ k}\Omega$ is the quantum resistance. Note that the number of conducting channels M strongly depends on the chirality, size, and temperature [34]–[36].

If we assume an uniform distribution of the current, i.e., $I(z, \omega) = J(z, \omega)X$, we can multiply both parts of (6) by X and rewrite it in spatial-frequency domain (using $\beta \rightarrow -\partial^2/\partial z^2$)

$$I(z, \omega) + \psi(\omega) \frac{\partial^2 I(z, \omega)}{\partial z^2} = \frac{\sigma_0 X}{1 + i\omega/\nu} E_z(z, \omega). \quad (9)$$

The second term on the left-hand side introduces a spatial and frequency dispersion, whereas the coefficient of the electric field introduces a frequency dispersion.

We assume the electromagnetic field to be low enough for using the linear approximation with respect to it (namely, for voltage values $V < k_B T/e$). Thus, it is possible to derive a simple linear TL model for the nano-interconnect schemes in Fig. 1 (e.g., see [28], [29], and [32]) by coupling (9) with Maxwell's

equations. Assuming a single line (one wire above the ground), we would have the TL equations

$$-\frac{dV}{dz} = (R_{\text{TL}} + i\omega L_{\text{TL}})I, \quad -\frac{dI}{dz} = i\omega C_{\text{TL}}V \quad (10)$$

where the per-unit-length (p.u.l.) resistance, inductance, and capacitance would be given by

$$R_{\text{TL}} = \frac{\nu L_k}{\Theta(\omega)}, \quad L_{\text{TL}} = \frac{L_k + L_M}{\Theta(\omega)}, \quad C_{\text{TL}} = C_E \quad (11)$$

where L_M and C_E are the p.u.l. magnetic inductance and electrostatic capacitance, respectively, and

$$\Theta(\omega) = 1 + \frac{C_E}{C_q} \left(\frac{\xi(\omega)}{1 - i\nu/\omega} \right) \quad (12)$$

$$L_k = \frac{1}{\nu\sigma_0 X} = \frac{R_0}{2\nu F M}, \quad C_q = \frac{1}{L_k v_F^2} = \frac{2M}{R_0 v_F}. \quad (13)$$

In (11)–(13), two novel terms appear with respect to the ordinary macroscopic TL equations: the p.u.l. *kinetic inductance* L_k , related to the mass inertia of the conduction electrons, and the p.u.l. *quantum capacitance* C_q , related to the quantum pressure arising from the zero-point energy of such electrons.

In spite of their different physical meanings, the *generalized* TL model with parameters (11), (12), to be valid for CNT lines and metallic NWs, is consistent with the classical TL model for a macroscopic line. To show it, we assume the simple case of a copper wire above the ground, with $D = 400 \text{ nm}$ and $H = 2D$ (see Fig. 1). For copper NWs, the number of channels M at room temperature may be calculated by $M \approx aS_W + b$, where $a = 0.111 \text{ nm}^{-2}$ and $b = 3.036$ [see [31] and (4)]. In this case, it is $M \approx 1.4 \times 10^4$. For such a case, it is $\Theta \approx 1$ and $L_k \ll L_M$, and so (11) and (12) yield the classical TL parameters: $R_{\text{TL}} = 1/(\sigma_0 S_W)$, $L_{\text{TL}} = L_M$, and $C_{\text{TL}} = C_E$.

Here, we meet an important difference between macroscopic and nanoscale TLs. For macroscopic TLs, the working mode is the transverse electromagnetic (TEM) wave, with propagation velocity $c = 1/\sqrt{LC}$. The working mode in nano-TLs is a surface wave with rather large longitudinal component; thus, from (13), we obtain $v_F = 1/\sqrt{L_k C_q}$. Such coupling condition between linear electric parameters should be taken into account in EMC applications at nanoscale.

The TL model presented earlier have been extended for multiconductor transmission lines (MTLs), where the currents and voltages are presented by vectors, while p.u.l. parameters become matrices. For operating frequencies up to THz range, it is possible to neglect both the tunneling and the overlap of electronic states in adjacent CNTs or NWs (e.g., see [37]). In this case, the kinetic and quantum terms are presented only by the on-diagonal elements of the parameter matrices, while the off-diagonal terms are mainly related to the mutual magnetic inductances and electrostatic capacitances. In other words, only electromagnetic coupling is considered. Finally, the circuit model should be completed by adding lumped terminal resistances, which account for the contact effects.

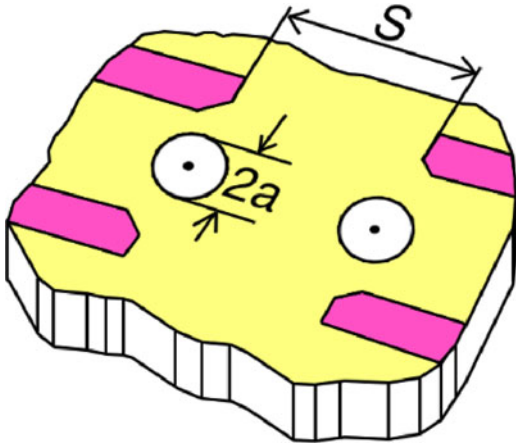


Fig. 2. Two quantum dots interacting with two nano-interconnects.

B. Modeling Quantum Devices

A challenge for nano-EMC is the study of large (multielement) quantum digital systems, with dramatically enhanced level of integration. As shortly mentioned in Section I, quantum computing has been proposed as a new paradigm for information transport, storage, and processing, promising a dramatic improvement of device integration and computational performance [38], [39]. Although a technology for quantum computing is still far from being defined and assessed, the recent literature provides many types of physical systems considered as candidates for basic digital elements of quantum origin. For instance, a possible way to implement the so-called *qubits*, at the basis for quantum computing, is given by the using of quantum dots, coupled via the phenomenon known as *quantum entanglement* [39], [41]. On the other hand, entanglement is able to manifest itself in the creation of parasitic couplings, unwanted from the EMC point of view. Therefore, it is of interest to introduce simple models for such quantum devices in the frame of the circuit theory. Here, we propose an equivalent two-port lumped model for the device depicted in Fig. 2, where a pair of quantum dots (QDs) is placed close to the terminations of two interconnects. Quantum devices show energy spectrum for operated steady states, characterized by wave functions localized in a finite spatial area via high potential barriers. The confinement region is approximately given by $A_{\text{eff}} \approx 4a^2$, where a is the radius of the QD (or the Bohr radius if the device is a single atom).

We consider a quantum device characterized by two energy states: in this case, only one type of transition may be resonant with an external EM field. Thus, we assume such a field to be monochromatic with frequency approximately equal to the transition frequency. In addition, we assume that the dimension of the confinement size $2a$ is electrically small at the given frequency; thus, the single quantum device may be modeled as a one-port lumped element. We indicate the voltage and the current intensity of the one-port element with $V(t)$ and $I(t)$, respectively. Following [42] and [43], the device equivalent impedance may be expressed in terms of the quantum

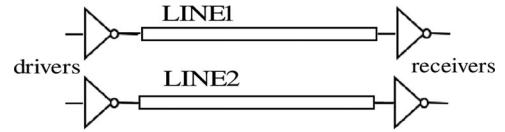


Fig. 3. Schematic of a two-channels signaling system.

polarizability $\alpha(\omega)$ as

$$Z_L(\omega) = \frac{V}{I} = \frac{i}{\alpha(\omega)\omega} A_{\text{eff}} \quad (14)$$

where following the Kubo approach [44], it is

$$\alpha(\omega) = \frac{1}{\hbar} \frac{2\mu^2\omega_0}{\omega_0^2 - \omega^2 + i\omega\gamma}. \quad (15)$$

In (14) and (15), ω_0 is the frequency of quantum transition between the two stationary states, μ is the dipole moment of the transition, and γ is the spontaneous emission decay.

One of the possible quantum coupling mechanism between the two lumped devices, for instance, exists via dipole–dipole interactions (another coupling mechanism is spin–spin interaction, etc.) [45]. As a consequence, the original two-level energy spectra of the uncoupled quantum devices are transformed now into a one-piece four-level one. In this case, two intermediate levels correspond to the so-called *entangled states* [39]: although only one quantum device is excited, this excitation is distributed with the same probability between both devices, due to quantum correlations [39]. It is necessary to distinguish between symmetric (*superradiant*) and antisymmetric (*subradiant*) states, which are characterized by different values of transition energies and emission decays [39].

The characteristic of the two ports representing the pair of quantum devices in the entangled states may be again found by using the Kubo approach [44]. For the symmetric state, we have

$$\mathbf{I}(\omega) = \mathbf{Y}(\omega)\mathbf{V}(\omega) = \frac{1}{2Z_L(\omega)} \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix} \mathbf{V}(\omega) \quad (16)$$

where $\mathbf{V} = [V_1, V_2]^T$ and $\mathbf{I} = [I_1, I_2]^T$ are the voltages and currents at the two ports, whereas $\mathbf{Y}(\omega)$ is the matrix of equivalent conductivity, and Z_L is given by (14).

III. COUPLING AND MATCHING AT NANOSCALE

In this section, we discuss the concepts of coupling and matching, referring to the simple two-channel signaling system in Fig. 3. In order to study the coupling, a typical condition is given by switching on only one driver (for instance which connected to line 1) and evaluating the induced voltages at the near and far end of the other line (line 2), usually normalized to the driver voltage. As for the matching, we will discuss the behavior of the reflection coefficient at the load section.

Here, we discuss two complementary cases: 1) two electromagnetically coupled NWs terminated with two classical uncoupled loads; 2) two uncoupled ideal transmission lines with quantum devices in entangled states.

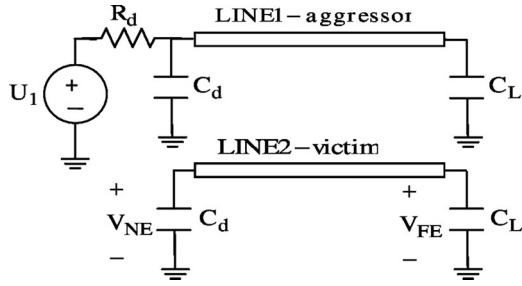


Fig. 4. Schematic of a two-line signaling system for crosstalk analysis.

A. Electromagnetically Coupled Nano-Interconnects

In this section, we consider for crosstalk analysis [46] the MTL in Fig. 1, used as a two-channel line in the circuit shown in Fig. 4. The drivers and receivers are modeled as real voltage sources and capacitors, respectively.

In macroscale modeling, the crosstalk voltages at the near and far ends of electrically short lines are simply given by [46]

$$\frac{V_{NE}(\omega)}{U_1(\omega)} = i\omega l(K^{\text{cap}}C_m + K^{\text{ind}}L_m) \quad (17)$$

$$\frac{V_{FE}(\omega)}{U_1(\omega)} = i\omega l(K^{\text{cap}}C_m - K^{\text{ind}}L_m) \quad (18)$$

where l is the line length, C_m and L_m are, respectively, the p.u.l. mutual capacitance and inductance of the line, and K are coupling coefficients related to the terminal impedances. The subscripts NE, FE relate to near-end and far-end voltages, whereas the superscripts cap and ind correspond to capacitance and inductance, respectively.

In the wide-separation approximation, the self and mutual terms of the inductance matrix \mathbf{L} for the MTL in Fig. 1 are [46]

$$L_s = \frac{\mu}{2\pi} \ln\left(\frac{2H}{D/2}\right), \quad L_m = \frac{\mu}{4\pi} \ln\left(1 + 4\frac{H^2}{S^2}\right) \quad (19)$$

whereas the p.u.l. capacitance may be evaluated by $\mathbf{C} = \mu\epsilon\mathbf{L}^{-1}$.

We start from a given set of values for the geometrical parameters D , H , S , and l that provide satisfactorily low crosstalk voltages [see (17) and (18)] for the considered frequencies and loads. In classical applications, this happens, for instance, by following the so-called “ $3W$ spacing rule,” i.e., by assuming the edge-to-edge distance between the signal traces (in this case, S) to be equal to three times the trace width W (here replaced by the diameter D). This is a common compromise between acceptable routing density and crosstalk [14]. We can define a scaling rule reducing the dimensions by the same factor x

$$D' = Dx, \quad S' = Sx, \quad H' = Hx. \quad (20)$$

After the scaling (20), the crosstalk noise is left unvaried, since the matrices \mathbf{C} and \mathbf{L} do not change, according to (19). If we scale down also the line length l , then the crosstalk noise is proportionally reduced. This simple scaling rule may be rigorously used for lossless lines and is approximately true for lossy lines too, if the internal inductance can be neglected.

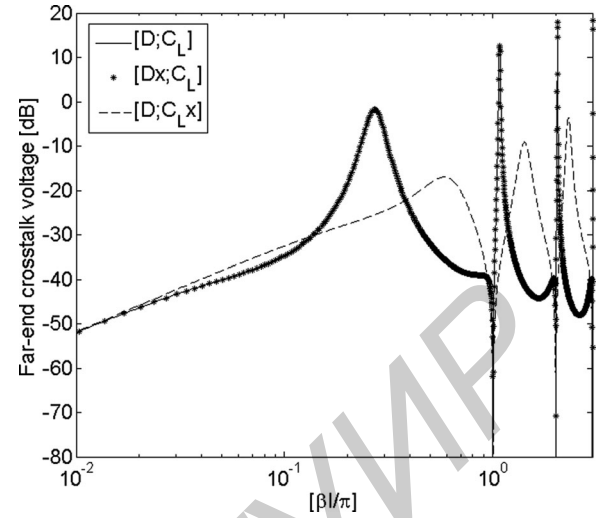


Fig. 5. Far-end crosstalk noise for the circuit in Fig. 4, assuming a classical TL model (two copper lines), after scaling the wire diameter D and/or the load capacitance C_L by a factor x .

The same behavior may be still found after removing the hypothesis of electrically short lines, hence evaluating the noise voltages as solution of a TL problem. Fig. 5 shows the amplitude of the far-end crosstalk voltage, obtained for a classical TL model (pair of copper wires), assuming for parameters defined in Fig. 1, the values $D = 0.4$ mm, $H = D$, $S = 3D$, and $l = 10$ mm. For the loads shown in Fig. 4, we take $C_L = C_D = 1$ pF and $R_D = 80$ Ω . The result obtained by using (20) with a factor $x = 10$ is the same, since the two curves coincide. The crosstalk noise shows a peak dependent on the value C_L and shifts to higher frequencies as C_L decreases. In addition, the solution exhibits the typical TL resonances for $\beta l = n\pi$. The line length shortening reduces the level of crosstalk and shifts the mentioned resonances to higher frequencies, enlarging the frequency range with negligible level of noise.

We now study the same problem for the nanoscale TL model (interconnect based on two CNTs). The geometry of the problem again corresponds to Fig. 1. We consider either a multiwall CNT of diameter $D = 20$ nm, or a metallic single-wall CNT with $D = 20$ nm. For other parameters, the chosen values are $H = D$, $S = 3D$, and $l = 0.1$ mm. The interconnect is used in a circuit like that in Fig. 4, with $C_L = C_D = 0.1$ pF and $R_D = 3$ k Ω . To take into account the contact resistance, an additional lumped resistor of $0.5 R_0/M$ is added at each termination. The far-end crosstalk noise is reported in Fig. 6, considering again the cases when C_L or D are reduced by a factor of 10.

As observed for the classical model, the reduction of the load capacitor shifts the peak of the noise to higher frequency values. The novelty is the sensitivity to the wire diameter that breaks the scaling rule observed in the classical solution. The reason is due to the impact of the number of conducting channels M on the kinetic inductance L_k and the quantum capacitance C_q [see (13)]. For low values of M , L_k is usually larger than the magnetic inductance; hence, the p.u.l. inductance matrix (which includes L_k only in the self terms) becomes diagonally dominant. This dominance depends on M , which, in turn, is

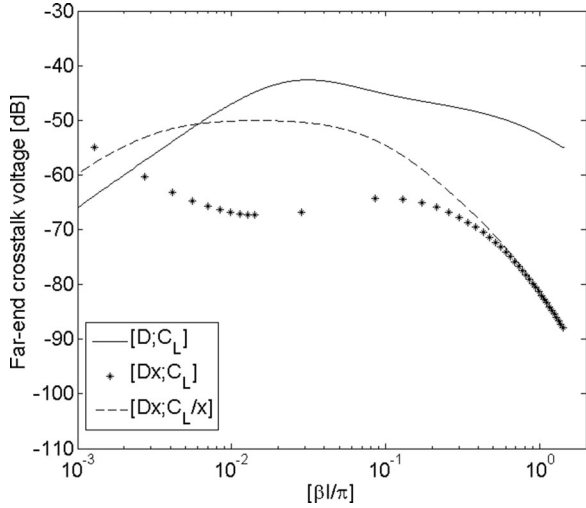


Fig. 6. Far-end crosstalk noise for the circuit in Fig. 5, assuming a nanoscale TL model (two CNT lines), after scaling the wire diameter D and/or the load capacitance C_L by a factor x .

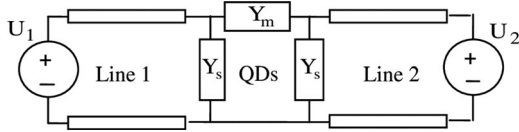


Fig. 7. Equivalent scheme for the two uncoupled lines terminated on two coupled quantum devices, represented as a π -type two-port. The admittances are $Y_s = Z_L^{-1}$, $Y_m = -(2Z_L)^{-1}$, where Z_L is given by (14).

related to the wire diameter and temperature [34]–[36]. In our case, at room temperature, we pass from $M \approx 20$ (for multiwall CNTs) to $M \approx 2$ (for single-wall CNTs). By increasing M , the bulk behavior is reached, while L_k and C_q become negligible. As pointed out in Section II-A, this happens for single metallic NWs or bundles of thousands of CNTs, when diameter D reaches the values of hundreds of nm or more. This is usually the case of practical applications of CNT on-chip interconnects; therefore, the mentioned phenomenon is not observed in the crosstalk analysis of such interconnects [47].

B. Pair of Quantum Devices in Entangled States

We now discuss the case of two uncoupled lossless TLs, fed by two ideal voltage sources and terminated with a pair of quantum devices in entangled states, as schematically depicted in Fig. 7. The lines are assumed to be identical, thus having the same wavenumber $\beta = \omega\sqrt{LC}$ and characteristic impedance $Z_C = \sqrt{L/C}$. The device is the pair of quantum dots (see Fig. 2) assumed to be in the superradiant entangled state so that (16) holds. As shown in Fig. 7, the device may be represented by a simple π -type two-port, derived from (16), with the self- and mutual admittance given by

$$Y_s = Z_L^{-1}, \quad Y_m = -(2Z_L)^{-1}. \quad (21)$$

Note that the coupling element Y_m has a negative real part, without contradicting the thermodynamic equilibrium. As noted

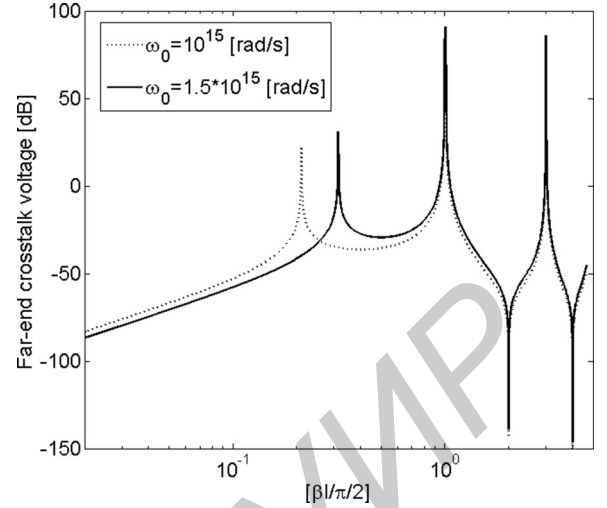


Fig. 8. Far-end crosstalk voltage for coupled quantum loads, for different values of the quantum transition frequency.

by Schrödinger [48], “The whole system can be less uncertain than either of its entangled parts.” It means that the whole equivalent circuit is better specified than its elements. In our case, a negative resistance of circuit element means that there is a special type of energy transfer inside the system, different from the outside energy supply. It strongly contradicts the intuitive concepts of classic crosstalk, in which the electromagnetic coupling should be described only by passive elements [12]–[14], [46]. For these reasons, the considered system is not equal to a pair of coupled harmonic oscillators and has no analogs in classical electrodynamics.

To study the circuit in Fig. 7, each line may be represented as a two-port network via the transmission matrix [46]

$$T = \begin{bmatrix} T_s & T_{12} \\ T_{21} & T_s \end{bmatrix}, \quad \begin{cases} T_s = \cos(\beta l) \\ T_{12} = -iZ_c \sin(\beta l) \\ T_{21} = -iZ_c^{-1} \sin(\beta l) \end{cases} \quad (22)$$

As in Section III-A, we evaluate the coupling by studying the voltage on the load Z_L of line 2, when $U_1 = 1$ V and $U_2 = 0$ V. By coupling these boundary conditions to line matrix (21), we obtain a simple expression for the far-end voltage

$$V_{FE} = \frac{1}{2} \frac{T_{12}}{T_s(T_{12} - Z_L T_s)} = \frac{1}{2} \frac{\tan \beta l}{\sin(\beta l) - i(Z_L/Z_C) \cos \beta l}. \quad (23)$$

In the following, we assume that each quantum device is made by the GaAs double quantum dot proposed in [49] as a qubit for quantum computing. We consider the following values for the parameters in (14)–(16): $a \approx 20$ nm, $\omega_0 \approx [1 \div 1.5] \times 10^{15}$ rad/s, $\gamma \approx 3 \times 10^{11}$ Hz, and $\mu \approx 7.59\hbar$ [3].

The frequency behavior of the far-end voltage is plotted in Fig. 8, with varying values of the frequency of quantum transition ω_0 . As a consequence of the entanglement, the active line is able to excite signals into the victim line even in absence of interline coupling. The spectrum plotted in Fig. 8 shows a

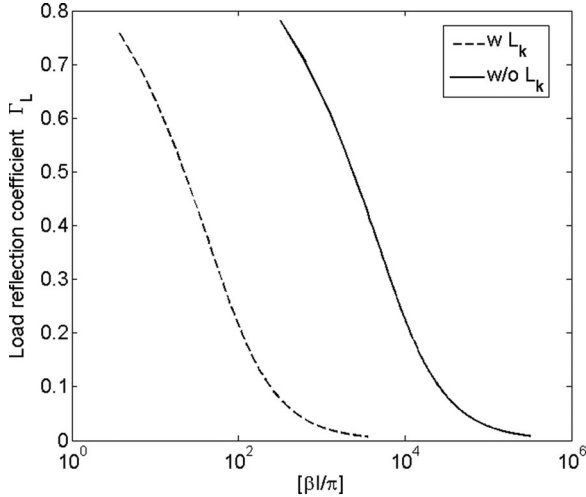


Fig. 9. Load reflection coefficient for a lossy nanotransmission line, with or without the effect of the kinetic inductance.

resonance for $\omega = \omega_0$, besides the classical resonances due to the transmission lines (for $\beta l = n\pi/2$).

C. Matching Conditions

In this section, we discuss the concept of matching, referring to a single transmission line made by one of the signal wires in Fig. 1 and the ground plane. In the classical TL theory, the amplitude of the reflection coefficient at the load section is given by [46]

$$\Gamma_L = \frac{1 - \zeta}{1 + \zeta}, \quad \zeta = \frac{Z_C}{Z_L} \quad (24)$$

which leads to the classical *matching condition*

$$Z_L = Z_C \quad (25)$$

giving $\Gamma_L = 0$. As it is well known, for a lossless line, the characteristic impedance becomes a pure resistance $Z_C = Z_{C0} = \sqrt{L/C}$; therefore, a resistive load $Z_L = Z_{C0}$ would give a perfect matching at any frequency. For a lossy line, the characteristic impedance becomes complex and frequency dependent. For instance, for the simple case of a lossy *RLC* line without skin effect, it is

$$Z_C(\omega) = \sqrt{\frac{R + i\omega L}{i\omega C}}. \quad (26)$$

It means that the load $Z_L = Z_{C0}$ would give a perfect matching condition only in the high-frequency limit ($\omega \rightarrow \infty$).

If we consider the nanoscale TL, the situation qualitatively changes: the frequency range of satisfactory matching may be enlarged as a consequence of the presence of the kinetic inductance L_k . Let us consider, for instance, a metallic single-wall CNT with $D = 2$ nm, $H = D$, and $l = 1$ mm. In this case, $L_k/L_M \approx 1.3 \cdot 10^4$ and $C_E/C_q \ll 1$. Fig. 9 plots the load reflection coefficient (24), evaluated with and without the contribution of L_k . If, for instance, in a given problem, a satisfactory matching can be considered when the reflection coefficient is

less or equal to 0.1, then from Fig. 9, it is evident that in the presence of kinetic inductance, the region enlarges where this condition is fulfilled.

As shown for the crosstalk analysis, this effect vanishes when the number of channels M is large enough to lower the value of the kinetic term (for large diameter NWs or large CNT bundles).

Let us now discuss the concept of matching when an ideal TL is ended with a pair of quantum devices in the entangled state (see Fig. 7). Assuming one of the two lines to be inactive, the reflection coefficient at the load of the other line may be expressed as

$$\Gamma_L = e^{3i\beta l} \frac{2e^{-i\beta l} \cos(\beta l) - \zeta}{2e^{i\beta l} \cos(\beta l) + \zeta}, \quad \zeta = \frac{Z_C}{Z_L} \quad (27)$$

which provides a new matching condition that redefines (25)

$$Z_L = \frac{Z_C}{2} (1 + i \tan(\beta l)). \quad (28)$$

If we would impose the classical matching condition (25), we would obtain an energy reflection coefficient $[\Gamma_L]^2 \in [0.1, 1.0]$, depending on the phase shift βl . Condition (28) imposes an optimal phase shift between the source and the load in order to obtain total absorption, whereby the matching impedance becomes complex and depends on the line length. Thus, we obtain another result, important from EMC point of view: quantum entanglement is able to break down the regime of matching between transmission line and the load.

IV. CONCLUSION

The new phenomena introduced by quantum effects in nanoelectronic systems suggest a deep revision of the concepts adopted in the classical EMC analysis. The phenomenological approaches based on separable description of physical properties of materials and electromagnetic response of electronic devices and systems become invalid on nanoscale. Instead, a self-consistent modeling of dynamics of quantum charge carriers and classical electromagnetic fields becomes necessary. The most efficient approach to this problem is based on the fundamental physical theory of generalized susceptibilities (Kubo approach).

In this paper, we analyzed two case studies: coupled nanoscale interconnects terminated with uncoupled loads and coupled quantum devices in the entangled state connected to two uncoupled interconnects. In both cases, the coupling and matching conditions are dramatically modified, as compared to the classical EMC theory.

As for the nano-interconnects, their equivalent electrical parameters are affected by kinetic inductance and quantum capacitance, which introduce a new behavior with respect to the dimension scaling. The classical scaling rules no longer hold, as well as the separation rules adopted to mitigate the crosstalk. The kinetic inductance, however, plays a beneficial role, enlarging the attainable frequency range of the satisfactory matching of the load with the line.

A pair of quantum loads coupled via entanglement has been considered. As a result of quantum coupling, a voltage arises in the passive line, in spite of its electromagnetic decoupling with

the active one. Thus, a novel concept arises: since the entanglement is a “spooky action at distance,” its effects may surpass those due to the near-field electromagnetic coupling, which are modeled by the cross-admittances. Quantum entanglement introduces a novel matching condition between the line and the load, with the optimal value of the load impedance dependent on the line length.

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